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FEDERAL COMMUNICATIONS COMMISSION
Washington, D.C. 20554

November 29, 2001

Ms. Magalie Roman Salas
Secretary
Federal Communications Commission
445 12th Street, S.W. TW-A325
Washington, D.C. 20554

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FEDERAL COMMUNICATIONS COMMISSION
OFFICE OF THE SECRETARY

RE: CC Docket No. 98-147/Ex Parte Presentation
CC Docket No. 96-98, Ex Parte Presentation
CC Docket No. 99-216, Ex Parte Presentation

Dear Ms. Salas:

On Tuesday November 27, and Wednesday November 28, 2001, Paul L. Marrangoni, of the Federal Communications Commission's Office of Engineering and Technology, attended a meeting of Focus Group 3 (FG 3) of the fifth Network Reliability and Interoperability Council (NRIC V) held at the Federal Communications Commission in Washington, D.C. The members of FG 3 in attendance were: Pete Youngberg (Sprint), John Unruh (Lucent), Philip Kyees (Paradyne), Massimo Saorbara (Globespan), Gary Tennyson (Bell South), Greg Sherrill (Verizon), Robert Beard (AT&T), Paul Donaldson (MCI Worldcom), Jamal Boudhauia (Qwest), Kevin Schneider (Adtran) David Rosensien (COVAD), Thomas Maudox (Texas Instruments) and the Chair of FG 3, Ed Eckert (Catena Networks). Elizabeth Yoekus and Arron Goldberger, the FCC's Common Carrier Bureau, and Jeffery Goldthorp of the FCC's Office of Engineering and Technology monitored the meeting.

NRIC V Focus Group 3 completed work on the white paper regarding the deployment of intermediate ADSL transceiver units (TUs) and related spectral compatibility issues regarding central office based DSL. Copy attached.

The group also discussed the parameters and values that should be used to ensure that a loop voice circuit is functioning properly.

There was also a discussion of effective working length (EWL) for copper loops.

In accordance with section 1.1206(b)(2) of the Commission's rules, 47 C.F.R. § 1.1206(b)(2), the original and 5 copies of this letter and attachment are being filed with for inclusion in the public record of the listed proceedings.

Sincerely,



Paul L. Marrangoni
Office of Engineering and Technology
Federal Communications Commission

No. of Copies rec'd
List A B C D E

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1 **NRIC-V - Focus Group 3**
2 **Wireline Network Spectral Integrity**
3 **Washington, DC; November 27, 2001**

NRIC5FG3/2001-072R8

4
5 **Contribution**

6
7 **TITLE: Updated DRAFT for the White Paper on Intermediate TUs**

8 **SOURCE: Editor' of Intermediate TUs White Paper**

9 **TOPIC: Intermediate TUs**

10 **DISTRIBUTION: Focus Group 3**

11 _____
12
13 **ABSTRACT**

14 This contribution contains the final updated draft of the white paper including the editor's final edits
15 without change marks. The contents are those agreed at the conclusion of the November 27-29, 2001
16 meeting.

17 _____
18
19

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NOTICE

This contribution has been prepared to assist NRIC-V Focus Group 3. This document is offered to the committee as a basis for discussion and is not a binding proposal. The contents are subject to change in any form after more study. Specifically, the right to add to, or amend, the statements contained herein is reserved.

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Remote Deployed DSL: Advantages, Challenges, and Solutions

A publication of the Network Reliability and Interoperability Council (NRIC)

November 25, 2001

Remote Deployed DSL: Advantages, Challenges, and Solutions

34 The following members of NRIC-V, Focus Group 3 dedicated their time and talent
35 to the development of this white paper:

36

37 Edward Eckert, Catena Networks, Chairman Focus Group 3

38 Philip Kyees, Paradyne, Chairman FG3 SC1

39 Massimo Sorbara, GlobeSpan, Chairman FG3 SC2

40

41 Brad Beard, AT&T

42 Jamal Boudhaouia, Qwest

43 Jim Carlo, Texas Instruments

44 Paul Donaldson, WorldCom

45 Gene Edmon, SBC

46 Thomas Maudoux, Texas Instruments

47 Harry Mildonian, Lucent Technologies

48 David Reilly, Rhythms

49 David Rosenstein, Covad Communications

50 Kevin Schneider, ADTRAN

51 Greg Sherrill, Verizon

52 Patrick Stanley, Elastic Networks

53 Gary Tennyson, BellSouth

54 John Unruh, Lucent Technologies

55 Pete Youngberg, Sprint

56 The members of FG3 owe special thanks to the following members of the FCC
57 staff for their assistance in the execution of FG3's tasks:

58 Young Carlson, FCC OET

59 Aaron Goldberger, FCC CCB

60 Kent Nilsson, FCC OET

61 Paul Marrangoni, FCC OET

62 Jessica Rosenworcel, FCC CCB

Remote Deployed DSL: Advantages, Challenges, and Solutions

63 Elizabeth Yockus, FCC CCB

Remote Deployed DSL: Advantages, Challenges, and Solutions

64

65

66

ABSTRACT

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68 This paper addresses the wireline network spectral integrity challenge created when DSL transceivers are
69 deployed at locations remote from the central office (CO) yet within the potential reach of CO-based
70 DSL transceivers.¹ It discusses background, technologies, architectures and major issues surrounding the
71 evolution of the telecommunications access network as they relate to remotely deployed DSL
72 transceivers and wireline network spectral integrity.

73 The paper aims to assist the FCC and the industry in managing this very complex and difficult problem
74 by promulgating a consistent understanding of the underlying issues. It offers options for possible
75 solutions for deployment of CO-based systems in the presence of remote DSL transceivers. This paper
76 does not address repeatered systems.

77 All of the members of NRIC-V Focus Group 3 agreed to the inclusion of all of the material in this paper.
78 There is no consensus, however, on the extent to which any of the benefits, challenges or possible
79 solutions will affect the industry's ability to provide the consumer with more advanced service choices
80 (type and supplier) while maintaining wireline spectral integrity in a competitive, cost-effective, and
81 business-driven manner.

82

¹ This problem has the potential to take on different forms as DSL transceivers are placed between RTs and the end user (e.g. FTTx, ONU or MTU architectures).

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83 **1. Introduction**

84 *1.1. Purpose and Scope*

85 The purpose of this paper is to provide the FCC and the telecommunications industry a compendium of
86 the background, technologies, architectures and major issues surrounding access network evolution as it
87 affects, and is affected by, wireline network spectral integrity.

88 The white paper approach was taken due to lack of consensus in NRIC-V Focus Group 3 on a single
89 solution to the problem created when DSL transceivers are deployed at locations remote from the central
90 office (CO) yet within the potential reach of CO-based DSL transceivers.²

91 It was agreed that the facts surrounding this problem could be included in such a paper, along with many
92 points of view (possibly conflicting) on options for possible solutions to the deployment of remote DSL
93 transceivers. Such an approach would assist the FCC and the industry in managing this very complex
94 and difficult problem by promulgating a consistent understanding of it.

95 This paper does not address repeatered systems.

96 *1.2. The Big Picture*

97 There is a fundamental conflict between two equally important, but opposing, interests: (1) exploiting the
98 business opportunity of migrating DSL transceivers closer to the customer, and (2) protecting the
99 viability of services provided by DSL transceivers located at the central office.

100 Deployment of remote DSL transceivers provides a service benefit to consumers and a business
101 opportunity to service providers. When deploying from a remote location, a larger percentage of the
102 residential customer base can be served by reaching customers that cannot be easily served directly from
103 the CO and higher data rates can be provided to customers for richer and more advanced services.

104 While it is desirable to migrate DSL transceivers closer to the customer, there exists a potential threat to
105 competition by doing so. When proposing possible resolutions to potential spectral compatibility
106 problems, the current investment in CO-based DSL equipment must be considered and weighed against
107 the benefits of the more robust and higher speed service offerings enabled by DSL transceiver migration.

108 When crosstalk from remotely deployed DSL transceivers is encountered, CO-based DSL transceivers
109 may exhibit significantly reduced performance or be rendered completely inoperable. This crosstalk may
110 be seen when customers, whose loops are in the same distribution cable, are served both from CO-based
111 and remotely deployed DSL transceivers. The rate of occurrence of this condition is not yet fully known.
112 Data from one region suggest that the rate of occurrence will be low; however, some are concerned that
113 the rate of occurrence could be significant since the particular architecture used and the deployment
114 plans going forward will have an impact on the rate of occurrence.

115 The foundations of wireline network spectral integrity are based on the premise that complete spectrum
116 management guidelines, when properly implemented, will reduce the occurrence of service degradations
117 to levels where such events can be remedied in a timely manner without requiring the dedication of
118 excessive resources to remedy the problems. As of the date of this paper standards for spectral integrity

² This problem has the potential to take on different forms as DSL transceivers are placed between RTs and the end user (e.g. FTTx, ONU or MTU architectures).

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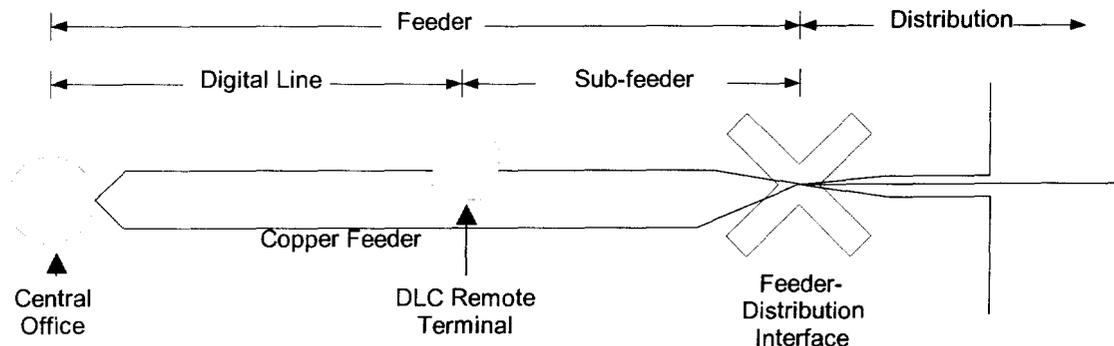
119 [1] assume network-side transceivers collocated in the central office; they do not include any additional
120 requirements associated with remote transceivers deployed to the same customer distribution area.
121 Currently, an issue 2 of the spectrum management standard is being developed that will address remote
122 deployment of network-side transceivers.

123 In summary, there is consumer value in CO-based DSL transceiver deployment as well as in migrating
124 DSL transceivers closer to the customer. In order for both to succeed, a framework must be established
125 to provide the consumer with more advanced service choices (type and supplier) while maintaining
126 wireline spectral integrity in a competitive, cost-effective, business-driven manner.

127 2. Access Architecture and Remote DSL Transceivers

128 Historically, the predominant access architecture involved the use of paired metallic cables. Starting in
129 the 1970's, loop carrier systems began to be deployed. These systems multiplex many customer services
130 onto a small number of transport lines. In the 1980's these carrier systems started employing digital
131 technology, and are denoted Digital Loop Carrier (DLC) systems. Please see Annex A for more details
132 on both DLC and metallic cable design practices and Annex B for loop architecture models.

133 In some cases, all of the circuits in an area are 'cut-over' to the DLC. There is no metallic path, of
134 whatever length, available to directly connect a potential user to the CO. In other instances, the DLC
135 transport parallels existing copper feeder cable. In these cases, a Feeder Distribution Interface (FDI,
136 sometimes referred to as a Serving Area Interface (SAI)) provides for connection to either the copper
137 feeder cable or the feeder circuits provided via DLC. This arrangement allows the service provider to
138 provide service to the customer via the copper plant or via the DLC remote terminal. Figure 1 portrays
139 this arrangement. Note that the FDI and the DLC remote terminal are often co-located.



140

141 **Figure 1: Dual Loop Architecture Reference Diagram**

142

143 The above architecture — involving both DLC and copper feeding the same FDI — permits DSL to be
144 deployed from the RT (remote DSL) or, if the copper feeder is short enough, from the central office.
145 Due to the difference in signal level between the two DSL transceivers, spectral compatibility issues may
146 arise when remote DSL is used to serve areas that can also be served via the copper feeder. This problem
147 is accentuated on longer loops when remote DSL transceivers are placed closer to the customer. This can
148 be the case when a remote DSL transceiver is placed in a Multi-Tenant Unit or in a curbside pedestal.

149 This Spectral Compatibility Issue will be defined further in Section 5.

150 **3. Benefits of Deploying Remote DSL Transceivers**

151 **3.1. Loop Limitations**

152 It is well understood that many customers cannot obtain Digital Subscriber Line (DSL) service.
153 Assuming that a DSL service provider is offering service from the Central Office (CO) from which the
154 potential DSL customer would be served, the reason that DSL is not available is in fact due to local loop
155 limitations. These limitations include the following:

- 156 • DLC deployments that preclude direct metallic access to the CO.
- 157 • The use of load coils, i.e., inductors spliced in series at periodic intervals on the loop in order to
158 maintain acceptable voice-grade quality.
- 159 • The loop over which the potential customer is served, although not loaded, is judged by the
160 potential service provider to be so long that there is a significant likelihood that the DSL circuit
161 will not operate successfully.

162 Each of these is explored in more detail below.

163 **3.1.1. Digital Loop Carrier**

164 DLC technology is often used to provide feeder facilities to an area. In some cases, all of the circuits in
165 an area are 'cut-over' to the DLC. There is no direct metallic path available to connect the potential DSL
166 customer to the CO. In this case, a remote DSL transceiver is the only means of providing the service.

167 In other cases, DLC technology is used to supplement the existing metallic feeder pairs. In these cases,
168 some or all of the existing metallic feeder pairs are left available, but 'growth' is served via the DLC-
169 provided feeder. In many of these cases, the area served is so far from the CO that DSL cannot be
170 supported on the metallic paired cable. Again, in such a case, deployment of a remote DSL transceiver is
171 the only means of providing the service.

172 **3.1.2. Loading**

173 Annex A provides a definition of loading. Most DSL systems cannot operate over loaded loops. Note
174 that loading coils generally exist only in the feeder portion of the loop. Where loops are short enough
175 such that loading is not required to ensure adequate voice grade performance, the load coils may be
176 removed to enable DSL service. Otherwise, a remote DSL transceiver connected to the FDI (hence,
177 beyond the last loading coil) is generally the only means of providing the service.

178 **3.1.3. Long, Non-Loaded Loops**

179 Successful DSL transmission, like any digital transmission scheme, requires that the DSL 'receiver'
180 enjoy some minimum Signal-to-Noise Ratio (SNR). This metric consists of two components, i.e., the
181 received signal level, and the noise level. As the loop gets longer, the received signal level drops. The
182 received noise is assumed to be due to crosstalk from systems on other cable pairs. The pair-to-pair
183 coupling provided by the crosstalk, though, is non-deterministic, i.e., some pair-combinations provide for
184 greater coupling than do other combinations.

185 Given that the noise coupled via crosstalk is an unknown, it can be seen that, as a loop gets longer, the
186 probability that a specific DSL system will enjoy some minimum SNR (and thus be capable of providing
187 an acceptable grade of service) diminishes. This factor, coupled with the variables in the wiring in a
188 customer's premises and the desire to maximize the ratio of successful installations, has resulted in a
189 decision by some service providers to 'disqualify' longer non-loaded loops.

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190 Again, in such a case, deployment of a remote DSL transceiver is generally the only means of providing
191 the service.³

192

193 3.2. Greater Data Rates

194 In addition to providing DSL service to those customers that could otherwise not obtain service, remote
195 DSL platforms provide a means to evolve broadband capabilities. Although DSL service might be
196 available, for instance, to a customer on a loop consisting of 14 kft of 26 AWG (American Wire Gauge)
197 cable, the resultant data rate may not prove to be satisfactory as the broadband access market matures.
198 While a customer might initially be satisfied with something less than 1 million bits per second (Mbps),
199 that data rate might not be satisfactory in a few years.

200 Because remote DSL transceivers are located at a point much closer to the customer (than from the CO)
201 the DSL service from the remote platform can be arranged to operate at a significantly greater data rate,
202 relative to that data rate that could be achieved from the CO. The data rate could be achieved through
203 exploiting the entire capacity of the mature Asymmetric Digital Subscriber Line (ADSL) technology, or
204 through the use of an evolving technology, such as Very-high-bit-rate Digital Subscriber Line (VDSL).

205 3.3. Summary of Remote DSL Advantages

206 In summary, remote DSL platforms provide the following two benefits:

- 207 • DSL service to those customers who could not otherwise obtain the service, and
- 208 • Higher data rates, relative to the data rate that could have been obtained via metallic paired cable
209 from the CO.

210 4. Challenges of Deploying Remote DSL Transceivers

211 The environment into which remote DSL transceivers are deployed presents several unique challenges to
212 service providers, including the following:

- 213 • Space – Remote cabinets and enclosures have space limitations that are not generally
214 encountered in Central Offices.
- 215 • Variety of services – Because remote locations do not have the size and scalability of Central
216 Office locations, the variety of DSL services that can be economically offered by multiple
217 service providers is limited.
- 218 • Backhaul of data – In some cases, there is insufficient data capacity between the CO and the RT
219 to adequately serve remote DSL deployments.
- 220 • Power – Remote locations are less likely to have excess reserve dc powering and battery backup
221 than Central Office locations.
- 222 • Craft access – Unlike Central Office equipment, Remote equipment is generally not in open
223 racks that can be easily accessed.

³ Some proprietary DSL implementations may provide for greater loop reach in this case than does standards-based ADSL. However, such implementations may not provide the data rate afforded by a remote DSL transceiver, or meet other service provider requirements.

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- 224 • Environmental requirements – Remote locations often require the use of environmental vaults or
225 temperature hardened equipment that is not needed for Central Office deployments.
- 226 • Economics – The smaller number of customers typically served by a remote location (as
227 compared to a CO) presents a challenge to the service provider's business case.
- 228 • Competitive access – Collocation space is generally less abundant in remote locations than in
229 CO locations.
- 230 • Voice switch access – It may be difficult to wire DSL equipment to voice switches and splitters
231 in a remote environment.
- 232 • Competitor's ease of connectivity - Cross-connection access to the incumbent's facilities may
233 not be readily available to competitors in a remote environment.

234 Another significant challenge to deployment of remote DSL transceivers is maintaining spectral
235 compatibility between the remote DSL and CO-based DSL. This spectral compatibility challenge is
236 discussed in detail in Section 5.

237 **5. Wireline Network Spectral Integrity Issues**

238 While there are advantages of delivering DSL service via remote platforms, there are some instances
239 where the remote DSL can cause significant interference into DSL being served from the CO. The
240 problem will primarily be seen when remote and central office deployments of ADSL serve customers
241 using the same distribution cable and the total loop length from the CO to the customer premises is short
242 enough (e.g. 15.5 kft EWL, or Equivalent Working Length, according to T1.417-2001[1]) to support the
243 affected DSL (namely ADSL).

244 For many remote DSL deployments, either because of the distance of the deployment from the CO or
245 because there are no copper facilities between the CO and the customer, this interference is not an issue.
246 In addition, when all of the service providers' DSL transceivers are deployed at the same remote
247 location, the existing spectrum compatibility requirements and assumptions from T1.417-2001 [1]
248 apply.⁴ However, there are currently no standards (i.e. Committee T1/T1E1.4) or regulations, which
249 prevent deployments where interference could be a significant problem. Given that remote deployments
250 of DSL are ongoing, it is important that the issues are understood and appropriate action taken. This
251 section provides a technical background of the issues involved.

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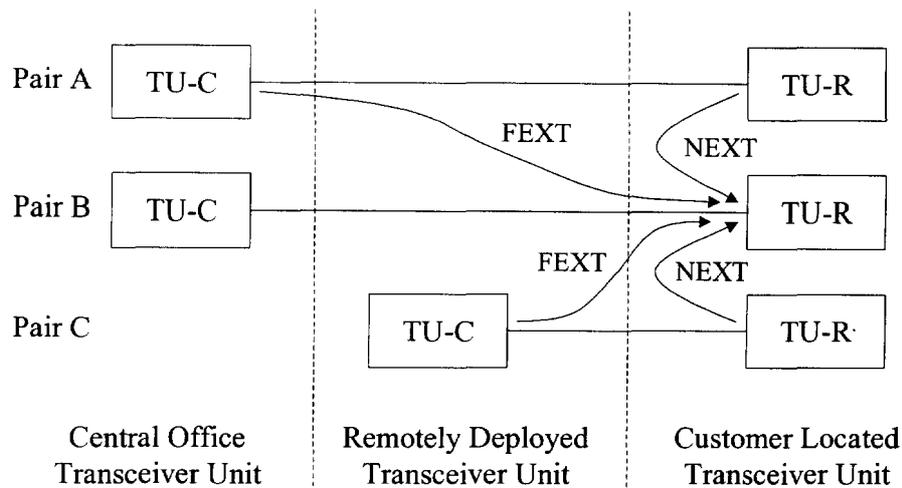
253 **5.1. Crosstalk and DSL performance**

254 Figure 2 shows a DSL deployment with multiple pairs in a single binder group. Two of the pairs, A and
255 B, run from the CO DSL transceiver to the customer located DSL transceiver while the third pair, C, runs
256 from a remotely deployed DSL transceiver to the customer located DSL transceiver.

257

⁴ This was proposed in T1E1.4/2001-060 [2] and agreed in T1E1.4 as new text for the next issue of T1.417-2001 [1].

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Figure 2: Model of remotely deployed transceiver units in a multi-pair cable.

260 The quality of the signal at the receiver limits the performance of DSL systems. Both the absolute
261 strength of the signal at the receiver, and the strength of the desired signal relative to the noise seen at the
262 receiver are critical to reception. The cable length and attenuation, along with the transmitter power,
263 largely determine the strength of the signal at the receiver. When multiple DSLs coexist in the same
264 binder group, crosstalk between pairs in the binder is a major source of noise, and a major limiter of
265 performance.

266 Crosstalk caused when the signal transmitted from the (CO and/or remotely deployed) TU-C of one pair
267 appears at the far end of another pair is called Far End crosstalk (FEXT). In Figure 2, the crosstalk
268 caused by the TU-C transmitters of pair A and pair C create noise which limits the ability of the
269 customer located TU-R receiver at the end of pair B to detect the signal intended for it.

270 Similarly, crosstalk caused when the signal transmitted from the (customer located) TU-R of one pair
271 appears at the near end of another pair is called Near End crosstalk (NEXT). In Figure 2, the crosstalk
272 caused by the TU-R transmitters of pair A and pair C create noise which limits the ability of the
273 customer located TU-R receiver at the end of pair B to detect the signal intended for it. NEXT can also
274 occur between TU-C's, for example between the TU-C's of pairs A and B in Figure 2.

275 DSL systems can be classified as frequency division duplex (FDD), echo cancelled (EC), and hybrid.
276 FDD DSL systems use different frequency bands for upstream (TU-R to TU-C) and downstream (TU-C
277 to TU-R) traffic. Echo cancelled systems use the same upstream and downstream frequency bands and
278 have echo cancellers to eliminate interference from the echo generated at the far end of the pair. Hybrid
279 systems have partially overlapping frequency bands in the upstream and downstream directions.
280 Frequency division duplex system performance is typically limited by FEXT, while echo cancelled
281 system performance is typically limited by NEXT.

282 5.2. Effect of DSL Transceiver Location

283 The effect of NEXT and FEXT on ultimate performance depends on the construction of the cable, the
284 relative location of the DSL transceivers, and on the type of DSL. Cable design can change both the
285 attenuation and the inter-pair coupling. As coupling between pairs increases, so does the crosstalk
286 experienced at the receiver. In Figure 2, the downstream DSL transmitter for pair C is much closer to the
287 receiver for pair B than the downstream transmitter for pair B. The cable for pair B attenuates the signal
288 from the Central Office located DSL transmitter to the customer located DSL receiver much more than

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289 the cable for pair C attenuates the signal from the remotely deployed DSL transmitter to the customer
290 located DSL receiver. Subscriber C may have better performance than subscriber B because of the
291 reduced attenuation and resulting stronger signal. Unfortunately, the crosstalk induced in pair B by the
292 downstream transmitter for pair C has similarly reduced attenuation. More FEXT is detected at the
293 receiver on pair B from pair C than is detected at the receiver on pair B from pair A. In some
294 deployments, the FEXT from pair C detected at the receiver from pair B may be nearly as strong as the
295 desired signal from the transmitter at the far end of pair B. In this case, the customer on pair B
296 experiences service that may have significantly reduced performance or may be rendered completely
297 inoperable.

298 **5.3. *The CO-RT crosstalk model***

299 When customers served from remotely deployed DSL transceivers (hereafter simply referred to as RTs)
300 using the same distribution cable as customers served from the Central Office (CO), the crosstalk
301 models⁵ are different than when all DSL transceivers are collocated. Compared to the case where all
302 service providers' DSL transceivers are deployed from the same location, the DSL transceivers at the
303 customer sites experience greater far-end crosstalk (FEXT) from the remote DSL transceivers than from
304 the CO-based DSL transceivers. See Annex C for a more complete description of FEXT and near-end
305 crosstalk (NEXT). Increased FEXT may occur when customers whose loops are in the same distribution
306 cable are served both from CO-based and remote DSL deployments.

307 **5.4. *Influence of DSL technology specific characteristics***

308 The effect of the RT crosstalk coupling is quite different depending on the spectral properties of the DSL
309 technologies that are involved. The increased FEXT coupling from the RT-based signals can
310 significantly reduce the level of performance (either in data rate capacity or bit error ratio) in the
311 downstream (CO-to-customer) direction for systems that are designed to have their performance limited
312 by the level of FEXT that is present. ADSL and VDSL are deployed as self-FEXT limited systems
313 because they use different transmit frequencies in each direction, a technique known as frequency
314 division duplexing. As a result, CO-based DSL transceivers may exhibit significantly reduced
315 performance or be rendered completely inoperable when significant FEXT coupling from RT-based
316 ADSL systems is present. This reduced performance has been documented in several T1E1.4
317 contributions, including T1E1.4/2000-302 [7] and T1E1.4/2000-336 [8].

318 Relatively unaffected by the increased FEXT coupling from remotely deployed DSL transceivers are
319 full-duplex DSL systems that use identical transmit spectra from both the service providers' and
320 customers DSL transceivers; it is self-NEXT that limits the performance of these systems.⁶ Because the
321 performance of these systems is limited by self-NEXT, the increased level of FEXT only slightly reduces
322 their performance. The NEXT coupling is still stronger than the increased FEXT coupling for most loop
323 lengths). This has been documented in T1E1.4/2000-240 [11] and T1E1.4/2001-081 [12].

⁵ A model showing the crosstalk coupling functions of interest is included in Annex L of T1.417-2001[1]. This model assumes that the pairs from the CO and RT share a binder group the entire distance from the RT to the customer. This assumption is a bit pessimistic. As shown in LA#5 of Figure 3 in Annex B (and in Figure 1 of Section 2), the FEXT from the RT-based TU-C is attenuated by the loss of the sub-feeder. The new model, which does include the effects of the sub-feeder, is shown in Annex C.

⁶ Examples of such systems include Basic Rate ISDN, IDSL (T1.601 [3]), HDSL (G.991.1 [4]), SDSL, and the versions of SHDSL with symmetric spectra (G.991.2 [5], T1.422 [6]).

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324 Affected to a greater degree than classical self-NEXT limited systems, but still less than ADSL, are the
325 full-duplex DSL systems, which use transmit spectra that are different in each direction but overlapped in
326 frequency.⁷ Remote deployment of these systems also affects the performance of CO-based ADSL more
327 than the classical self-NEXT limited systems.

328 Documentation of the effect that RT-based ADSL has on HDSL2 has been provided in T1E1.4/2001-081
329 [12].

330 5.5. *Influence of loop plant design (or architecture) on expected rate of incidence*

331 The expected rate of occurrence of CO and RT-based xDSL sharing the same distribution cables is
332 dependent on loop architecture. Since the affected distribution area must be served from both the remote
333 location and the CO, the problem is more likely to be seen where the remote platform has been added to
334 reinforce the loop plant originally served from the CO.

335 Several T1E1.4 contributions have addressed the issue of how likely this is to occur. In T1E1.4/2001-
336 069 [13] and in contributions to NRIC-V FG3, BellSouth reported that in their loop plant, less than 7%
337 of the loops working through a Feeder-Distribution Interface (FDI) and within 15 kft of the CO are
338 served via DLC. For this particular loop plant, this number represents an upper bound on the percent of
339 loops that have the potential to see this problem. T1E1.4/2001-179 [15] provides a similar analysis, using
340 data from a 1990 survey of 126 wire centers in five regions (T1E1.4/2001-132)[14], finding 12 to 18% of
341 loops eligible for remote DSL deployments are within 15.5 kft, and thus candidates for the crosstalk
342 problem. When presented, several expressed concern that, since the data was 10 years old, quite a small
343 sample, and did not include the impact of recent DSL deployments such as SBC's "Project Pronto", the
344 analysis was not necessarily reflective of the current loop plant. These studies may not necessarily
345 represent the impact of all future loop plant deployment architectures. For example, VDSL (which is
346 very likely to be deployed from a remote location) has not been considered.

347 6. Possible Solutions to the Spectrum Compatibility Challenge of Remote DSL

348 In the previous sections, we detailed the problem created when DSL transceivers are deployed at
349 locations remote from the central office (CO) yet within the potential reach of CO-based DSL
350 transceivers. In this section, we discuss possible solutions to this problem.

351 Within NRIC-V FG3 there was unanimous agreement that where spectral compatibility problems occur
352 due to the presence of remotely deployed DSL transceivers, a resolution to the problem needs to be
353 available. However, there was disagreement on whether these solutions would be employed as a reaction
354 to reported problems (reactive), or whether, as in the guidelines of T1.417-2001 [1], these solutions
355 would be employed in a proactive manner, with the intent to keep spectral compatibility problems to a
356 minimum. In this context, we define the following:

- 357 • Proactive means taking steps to assure that agreed-to analytical performance targets, such as
358 those in T1.417, can be met on a CO-based DSL circuit such that the CO-based DSL circuit is
359 unlikely to become impaired by crosstalk originating from the remote DSL transceiver.
- 360 • Reactive means taking steps to mitigate the effects of crosstalk from the remote DSL platform,
361 after these effects have resulted in degradation below the agreed-to performance targets of the
362 CO-based DSL circuit.

⁷ Examples of such systems include HDSL2 (T1.418 [9]), HDSL4 (T1.418 issue 2 [10]) and the versions of SHDSL with asymmetric spectra (G.991.2 [5], T1.422 [6]).

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363 Note that both proactive and reactive approaches could be applied on an "as needed" basis.
364 There was also no consensus on which party should be responsible for implementing solutions in either
365 case.
366 Because of the wide variety of loop architectures and their impact on the spectrum compatibility
367 problem, NRIC-V FG3 was unable to reach consensus on a one-size-fits-all solution. This section
368 outlines pros and cons of the potential technical solutions that were discussed within the group.
369 Note that the solutions described below should not be considered an exhaustive list; other solutions may
370 be possible.

371 **6.1. Technical Solutions using PSD-Based Approaches**

372 The spectrum compatibility problem we have been discussing is caused by the presence of greater FEXT
373 from the remotely deployed DSL transceiver than the FEXT-limited CO-based DSL transceiver was
374 expecting. Because the characteristics of the cable cannot be changed, a solution to this problem
375 involves adjusting the power and/or power spectral density of the DSL transceivers in such a way so that
376 the power of the signals at the RT are all approximately the same. This can be done with one of two
377 basic approaches (also referred to as categories):

- 378 (a) Set the power of all signals at the RT (or equivalent points in the feeder) at standard transmit-
379 levels. This can involve amplifying CO-based signals and/or moving the appearance of all
380 ADSL⁸ transceivers to the RT via RT collocation or derived logical circuits. This approach is
381 applicable in either a reactive or proactive manner.
- 382 (b) Lower or Alter the PSD of RT based systems so that they do not adversely affect CO-based
383 ADSL systems. While this approach may be used in both reactive and proactive approaches, the
384 reactive approach is most likely.

385 **6.1.1. Discussion on category (a)**

386 Solutions that fall into category (a) either involve competitive access at the RT site or some sort of
387 amplification of the CO-based ADSL signals at or near the RT so that the signal is of the same strength
388 as the RT-based ADSL. Possible solutions to competitive access at RT sites include the following:

- 389 • Traditional physical collocation (namely using the loop providers enclosure)
390 • Separate cabinets or enclosures
391 • The concept of "Open backplane" or line card collocation
392 • Unbundled virtual circuit

393 In general, amplifiers introduce additional spectrum management concerns. However, for the particular
394 case of resolving spectrum management issues at the RT, amplifiers may be attractive. Amplifiers
395 provide the RT-deploying service provider a way to "fix" any affected CO-based ADSL circuits, without
396 getting involved in the actual modem signal processing, and the associated interoperability difficulties.
397 There is a concern that such a solution is not scaleable. Difficulties related to this solution include
398 finding a suitable location for the amplifiers and providing power to this location, which in many cases is

⁸ ADSL is commonly referred to in this context, since it is a well-known and understood FEXT-limited DSL transceiver technology. Other FEXT-limited DSL transceiver technologies, including, but not limited to, VDSL, would be treated in a manner similar to ADSL.

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399 not located at the RT-site, but rather at an equivalent spot on the CO-FDI feeder route. (See Annex B,
400 Figure 3, loop architecture LA#5).

401 The solutions in this category provide an opportunity for RT-deploying service providers to
402 accommodate the affected CO-based circuits of other service providers, without affecting the
403 performance of their own deployments. Much of the discussion concerning these solutions revolved
404 around who would pay for the solution and whether it would have to be provided for only existing
405 affected ADSL circuits, or future CO-deployments as well (i.e. circuits that might be turned up in the
406 future using equipment already deployed, or even new deployments of equipment in the COs). This last
407 item was a subject of much disagreement and was the downfall of a proposed agreement.

408 There was also discussion concerning a different idea that has been adopted by the Australian network.
409 The idea here is that spectral compatibility for all DSL deployments would be determined from a defined
410 "deployment reference point" (DRP). In Australia, the DRP could be at any feasible interconnection
411 point along the loop. It is believed that when a service provider desires to deploy DSL at an intermediate
412 interconnection point (e.g. at a RT site), some form of policy exists which enacts a defined set of
413 procedures to move the DRP to that remote deployment closest to the customer. Once a deployment has
414 been made at an RT site, FEXT-limited systems deployed from "upstream" locations are deployed at
415 their own risk; all attempts at being spectrally compatible with them are ended. Concerns about this
416 approach include:

- 417 • How service providers would be notified about the change in DRP,
- 418 • Whether service providers would have input into the decision to change the DRP,
- 419 • How much time service providers would have to modify their deployments to operate in the new
420 environment,
- 421 • How effectively competitors could deploy in progressively smaller service areas as the DRP
422 moves closer to the customer, and
- 423 • Additional stranded investment at RT(s) behind the DRP, as well as at the CO.

424 **6.1.2. Discussion on category (b)**

425 Several solutions that fall into category (b) have been investigated and the results presented in T1E1.4.
426 They have involved lowering of the entire power spectral density (PSD) mask (T1E1.4/2000-321 [16]),
427 lowering portions of the PSD mask (T1E1.4/2000-321, 2001-080, -159, -160, -161 [16] through [20]) and
428 limiting the maximum excess noise margin of deployed ADSL systems. (T1E1.4/2001-136, -137 [21]
429 and [22])

430 All of these methods have been shown to reduce the amount of FEXT from RT-deployed ADSL into CO-
431 deployed ADSL circuits. However, most of the techniques cannot be implemented using the currently
432 deployed RT-based ADSL transceivers. Also, interoperability with the multitude of ADSL CPE modems
433 appears to be problematic. More technical work is required to determine if viable solutions can be
434 developed.

435 **6.2. Alternate Technology Solutions**

436 DSL service from the CO to the customer could also be provided through the use of an alternate DSL
437 technology that is relatively insensitive to the increased crosstalk due to the RT deployment (see 5.5).

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438 This capability could be provided at the CO through the use of interworking devices⁹. Solutions of this
439 type could be applied in either a proactive or reactive manner.

440 Solutions that fall into this category include:

- 441 • Those that employ a pair of interworking devices (one at the CO and one at the customer
442 location) to digitally transport both the POTS signals and DSL payload to the customer location
443 where the CO-based interfaces are re-created, and
- 444 • Those that employ a dual-mode customer modem (ADSL plus alternative DSL technology) and a
445 single CO-based interworking device (alternate DSL technology), operating in the frequencies
446 above the voice band, to transport the ADSL payload using the alternate DSL technology.

447 These solutions can be implemented quickly when deployed on a line-by-line basis. However, while
448 these solutions reliably provide broadband service, the data rates provided may not be as high as those
449 offered by CO-based ADSL in the absence of RT deployments. Therefore, these solutions may only be of
450 value on longer CO-based loops, where the alternate DSL technology can accommodate the lower ADSL
451 target rates. There are concerns about costs and operational issues; there are also concerns with who
452 would pay for the solution and whether it would have to be provided only for existing affected ADSL
453 circuits, or future CO-deployments as well.

454 **7. Summary**

455 This paper has provided information on the background, technologies, architectures and major issues
456 surrounding telecommunications access network evolution as it affects, and is affected by, wireline
457 network spectral integrity. It specifically addressed the wireline network spectral integrity challenge
458 created when DSL transceivers are deployed at locations remote from the central office (CO) yet within
459 the potential reach of CO-based DSL transceivers.¹⁰ It also offered options for possible solutions to the
460 deployment of remote DSL transceivers.

461 Within NRIC-V FG3 there was unanimous agreement that where spectral compatibility problems occur
462 due to the presence of remotely deployed DSL transceivers, a resolution to the problem needs to be
463 available. However, there was disagreement on the following issues:

464 1) Whether these solutions would be employed

- 465 In a reactive manner, which implicitly assumes that the probability of a spectral compatibility
466 problem is low, or
- 467 In a proactive manner, where solutions would be employed per the guidelines of T1.417-2001 [1]
468 for CO-based DSL transceivers with the intent to keep spectral compatibility problems to a
469 minimum.

470 2) Given the impact of the reactive solution on the customer of the CO-based service provider, what
471 probability of a spectral compatibility problem is "low enough" to make the reactive solution broadly
472 acceptable?

⁹ An interworking device translates between ADSL (possibly along with voice) and an alternative DSL technology.

¹⁰ This problem has the potential to take on different forms as DSL transceivers are placed between RTs and the end user (e.g. FTTx, ONU or MTU architectures).

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- 473 3) If the reactive approach is taken, would the service provider deploying the remote DSL transceivers
474 (RT) be required to accommodate (i.e. ensure no disruption of service to) only those CO-based DSL
475 transceivers installed at the time of the RT deployment, or would that party be responsible for all
476 CO-based DSL transceivers, including those installed at any time after the RT deployment?
- 477 4) Which party would be responsible for the costs involved in providing proactive or reactive measures,
478 either at the time of deployment or at any time after the deployment?

479 Because of the wide variety of loop architectures and their impact on the spectrum compatibility
480 problem, NRIC-V FG3 was unable to reach consensus on a one-size-fits-all solution.

481 The paper aims to assist the FCC and the industry in managing this very complex and difficult problem
482 by promulgating a consistent understanding of it.

483

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529

530 NOTE:

- 531 • Published and pre-published T1 Standards may be obtained at:
532 <http://www.t1.org/html/standard.htm>
- 533 • Contributions to Working Group T1E1.4 are public documents however the readers
534 attention is called to the “NOTICE” at the bottom of each contribution. These
535 documents may be obtained at: <http://www.t1.org/filemgr/filesearch.taf>
- 536 • Published versions of ITU-T Recommendations may be obtained at: <http://www.itu.org>

537

538

539

Annexes

A. Evolution of the Loop Architecture

A.1. Overview

542 The access network consists of the outside plant cable infrastructure and the drop that connects the cable
543 to the premises wiring. Historically, outside plant cabling has been designed to support the transmission
544 of voice grade signals with a useful bandwidth of between 3 and 4 kHz. The transmission path
545 historically consisted of metallic paired cable. In the past decade, use of optical fiber has become a
546 significant means of providing for new growth and for new services.

547 Metallic cable consists of pairs of solid copper conductors that are twisted together into units called
548 pairs. During manufacturing, several pairs, usually in 25 pair complements (also called binders), are
549 twisted together as separate bundles and the bundles are twisted together and wrapped in a polyethylene
550 and aluminum jacket. When signals are transmitted across a pair, an electromagnetic field is created
551 around the pair that is induced into other pairs in the same cable. As a result, a portion of the signal
552 appears on neighboring pairs. This effect is called crosstalk. The greatest effect of crosstalk is within
553 the same bundle. The twisting of the pairs and bundles tends to minimize coupling. However, the cable
554 design was intended to minimize crosstalk around voice frequencies. DSL technologies use frequencies
555 above the voice band. As the signals in copper cables increase in frequencies, crosstalk between pairs
556 also increases. Simulation models that characterize this phenomenon are used to evaluate the effect of
557 crosstalk on other services.

558 Optical fiber cable is also increasingly being used in place of metallic cable. Fiber is used because of its
559 generally lower cost per line, greatly increased bandwidth capability, and lower maintenance costs than
560 traditional copper plant. DSL applications generally permit much higher data rates when provided over
561 facilities that include fiber.

562 The design of telephone cables between the local wire exchange and the customer is referred to as
563 Outside Plant Design. Over the years, several sets of design rules for metallic cable have evolved. Many
564 of the rules were developed before divestiture of AT&T in 1983, so there is a fair degree of consistency
565 in their application throughout the country. Some variations will be noted in this document. This
566 description is not exhaustive but is intended to cover the most common designs that are still in use today.
567 It also describes some of the ramifications of using DSL bandwidths over voice-grade cable.

A.2. Resistance Design

569 The conductors in metallic cable vary in thickness, or gauge. They typically range from 26 and 24 AWG
570 (American Wire Gauge) for shorter cables to 22 and occasionally 19 AWG for the longest cables. Use of
571 the minimum gauge necessary, to control the voice band loss to an acceptable level, results in the most
572 economic design. Use of finer gauges for customers close to the central office is economical, allowing
573 lower cost per loop and allowing higher densities of customers served in the same cable and over the
574 same infrastructure of underground conduit, public and private easements, and pole lines. A simple way
575 to implement this efficiency was through the use of Resistance Design rules. These rules allow a

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576 maximum of 1300 Ohms loop resistance¹¹. For 26 AWG, this equates to about 15 kft, assuming a cable
577 temperature of 90 degrees F. For longer loops, combinations of gauges are used that keep the total
578 resistance within the 1300-Ohm limit. For non-loaded loops, the embedded base generally consists of 26
579 AWG out to about 15 kft and consists of a combination of 26 and 24 AWG from 15 kft out to the non-
580 loaded loop limit. Resistance design also includes rules for permitting bridged taps. A bridged tap is any
581 portion of the loop that is not in the direct path between the customer and the central office. For
582 example, if a loop serving a particular home also extends beyond the home to the end of the street, that
583 extension would be called a bridged tap. Bridged taps are commonly not limited to a single loop, but are
584 consistent throughout the binder. An exception is noted for situations where the extension of a single
585 loop beyond a customer terminal is sometimes removed to control bridged tap. In resistance design, any
586 number of bridged-taps is allowed with a maximum combined bridged-tap length of less than 6 kft.
587 According to loop surveys, most bridged taps are relatively short. In general, longer bridged taps have
588 the greatest impact on voice frequency while shorter bridged taps have the greatest impact on ADSL
589 frequencies.

590 Even with control of cable gauge and bridged-tap length, losses increase with frequency. For this reason,
591 loops over 18 kft require inductors, commonly called load coils^{12,13}. To reduce this loss near the
592 telephony voice upper-band edge, inductors can be inserted in series with the loop at periodic intervals to
593 reduce and flatten the voice-band loss. The first coil is placed at 3 kft from the central office and
594 additional coils are placed every 6 kft thereafter. A minimum of 3 kft (12 kft maximum) is required
595 between the last load coil and the customer. While load coils flatten the voice band attenuation
596 response, it is at the expense of increasing attenuation above 3 kHz. This increase in attenuation makes
597 DSL transmission over loaded loops difficult, if not impossible for most technologies. Loading coils are
598 placed on cables in increments of 25 pair binders.

599 ***A.3. Outside Plant Infrastructure***

600 Most cable plant designed in the last few decades is divided into feeder and distribution plant. Feeder
601 plant extends from the wire center to a location that permits cross-connects to the distribution plant.
602 Feeder cable is usually pulled through underground conduit in urban locations. Splice locations are
603 accessible to permit splicing unused segments of one cable to other cables that need additional capacity.
604 Bridged taps appear only occasionally on feeder cable. Distribution plant extends from the cross-connect
605 box to the premises. It is not designed to be as flexible for rearrangements as feeder plant. This is
606 because distribution plant is near the customer and must accommodate placement under sidewalks,
607 fences, driveways and foliage. Rearrangements are usually disruptive and expensive. For this reason,
608 distribution cable is sized so customers can order more than one line without need to rearrange the cable.
609 Typically, this flexibility is enabled by use of bridged taps. Since the loop provider does not know how
610 many lines a particular customer premises will require, bridged taps permit the same loops to pass by

11 Many service providers use a set of rules called Revised Resistance Design (RRD) to determine loop gauge. While rules have changed over time, the current rules allow a maximum of 1300 ohms loop resistance for nonloaded loops and a maximum of 1500 ohms for loaded loops.

¹² In the past loading rules for some services, such as PBX trunks, required the application of two load coils on some loops less than 18 kilofeet in length.

¹³ Additionally, single load coils are occasionally found on loops that were originally properly loaded, but at sometime in the past were re-arranged to serve an area closer to the CO. Apparently, for whatever reason, some of the load coils were not removed at the time of re-arrangement.

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611 several homes so that additional lines are available to whoever needs them. A Feeder-Distribution
612 Interface (FDI) is used to connect feeder and distribution loops to form a working line between the wire
613 center and the customer. In certain kinds of outside plant construction, the FDI is denoted as a Serving
614 Area Interface (SAI).

A.4. Carrier Serving Area Design

616 In the early 1980s, Carrier Serving Area (CSA) rules were written for the design of distribution cable.
617 CSA rules were originally written to enable the deployment of certain types of services without having to
618 condition the loops. These services included voice grade specials, Digital Data Service, and switched 56
619 kb/s services. CSA rules allow a maximum of 9 kft for loops that contain any 26 AWG and allow a
620 maximum of 12 kft for loops that contain only 24 AWG or coarser. A maximum of two bridged taps are
621 allowed. A single bridged tap cannot exceed 2 kft and the combination of both bridged taps cannot
622 exceed 2.5 kft. CSA bridged tap rules were intended to maximize voice-band performance; they do not
623 address those bridged tap lengths that have the most impact on ADSL performance.

624 With the advent of DSL technologies, these rules were used to define performance objectives in the
625 standardization process. Specifically, High-bit-rate Digital Subscriber Line (HDSL) (and its later
626 versions) was designed to work on CSA loops. Performance objectives were also established for ADSL
627 operating over CSA loops.

A.5. Digital Loop Carrier

629 In the 1980s, loop providers began provisioning access lines using a technology called Digital Loop
630 Carrier (DLC). DLC was provisioned in place of new copper cables to provide for subscriber line
631 growth. DLC entails the provisioning of channelized T-1 lines from the central office to a remote
632 location near the FDI. A Central Office terminal (COT) is placed at the central office end and a Remote
633 Terminal (RT) is placed near the FDI. The T-1 lines are repeatered every few kft. The length between
634 repeaters varies with cable gauge and whether the upstream and downstream channels are in the same
635 binder, adjacent binders, or non-adjacent binders. They carry time division multiplexed channels that
636 carry voice grade (up to 3.4 kHz bandwidth) traffic. The terminals at each end multiplex and
637 demultiplex traffic.

638 The DLC system described above is called a Universal DLC system. Later improvements replaced the
639 T-1 lines with optical fiber and integrated the COT into the central office switch. In the 1990s, another
640 improvement called Next generation Digital Loop Carrier (NGDLC) was deployed that uses time slot
641 interchange (TSI) to make more efficient use of the channels during quiet periods. More recently,
642 advances have been made to permit both DSL and voice over the DLC.

A.6. Enclosures

644 DLC systems typically employ battery backup. Early RT's (and their associated batteries) were typically
645 deployed in pedestals and pole-mounted cabinets. As the demand for larger systems developed, RT's
646 were deployed in huts and Controlled-Environment Vaults (CEV's). As the deployment of fiber moves
647 closer to the customer, e.g., in Fiber To The Curb (FTTC) systems, the number of customers served via
648 one remote site is smaller, thus resulting in smaller enclosures. These enclosures are designed to house
649 the equipment that is planned for a specific forecast period, and thus there is often no space to
650 accommodate unplanned equipment additions.

A.7. Dual Provisioning with DLC and copper

652 In some instances, DLC transport parallels existing copper feeder cable. At or near the RT, an FDI
653 provides for connection to either the copper feeder cable or the feeder circuits provided via DLC. This

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654 arrangement allows the service provider to provide service to the customer via the copper plant or via the
655 DLC remote terminal. This architecture permits DSL services to be served from the RT or, if the copper
656 feeder is short enough, from the central office. Spectral compatibility issues may arise when remote
657 DSL is used to serve areas that can also be served via the copper feeder.

658 See Figure 1 in Section 2 and LA#5 in Annex B for pictorial representations of this arrangement.

659 As loop architectures continue to evolve, concerns for wireline spectral integrity will continue.

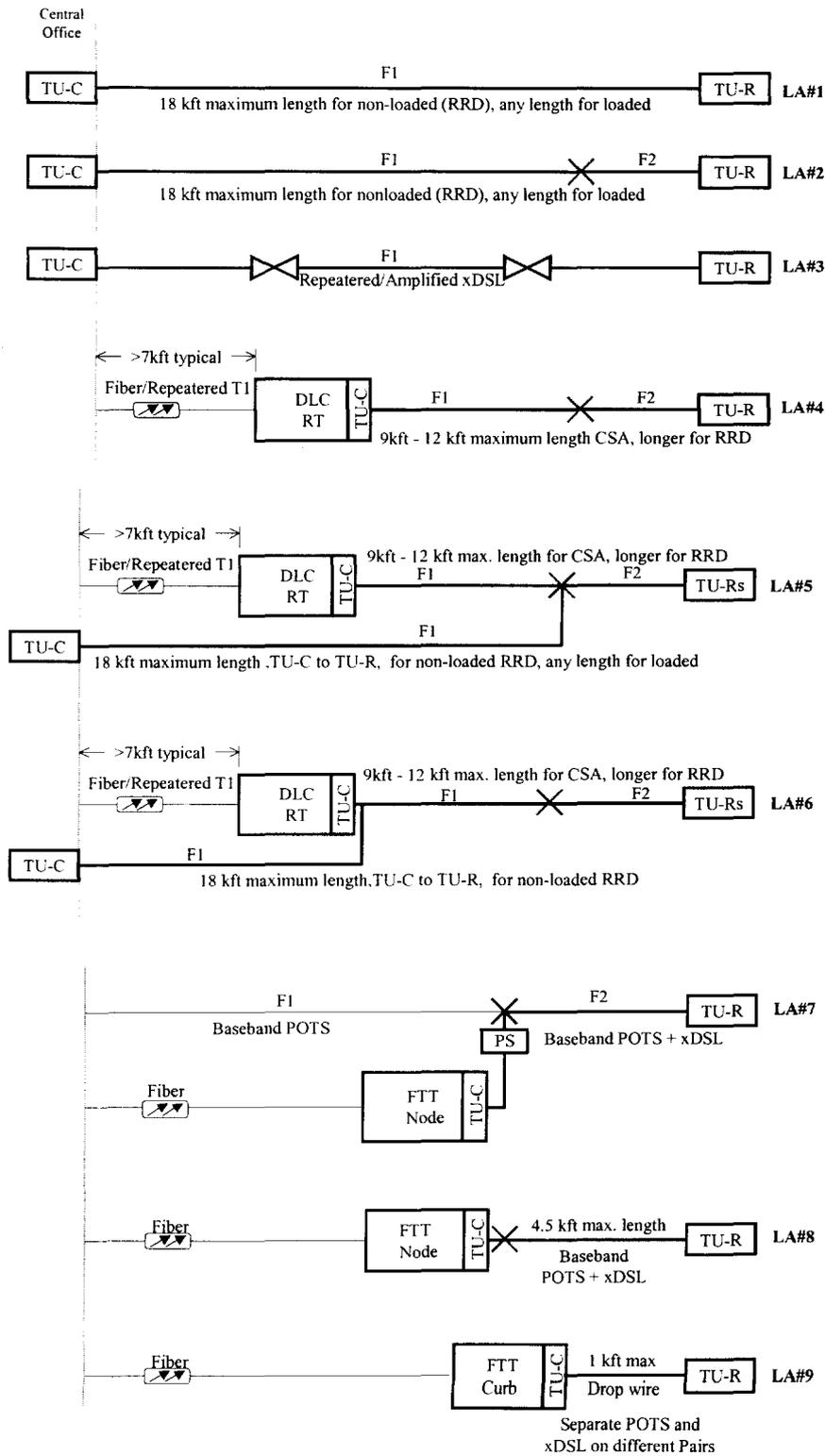
660 B. Loop Architectures

661 This Annex describes the various DSL loop architectures, including remote TUs and repeaters. The loop
662 architectures described include DSLs deployed

- 663 • Using direct metallic access from the CO
- 664 • With repeaters or amplifiers in the loop
- 665 • In or near RT cabinets at intermediate points in the loop plant, and
- 666 • At fiber ONUs at intermediate points in the loop plant or near the customer premises.

667 Figure 3 shows the different possible loop architectures.

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668

669

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671

672

Figure 3: DSL Loop Architectures (LA).

673

674 **C. Crosstalk Simulation Models**

675 *C.1. Crosstalk in the Loop Plant*

676 Crosstalk generally refers to interference that enters a communication channel, such as a twisted wire
 677 pair, through some coupling path. The diagram in Figure 4 shows two examples of crosstalk generated
 678 in a multi-pair cable. On the left-hand side of the figure, signal source $V_j(t)$ transmits a signal at full
 679 power on twisted wire pair j . This signal, when propagating through the loop, generates two types of
 680 crosstalk into the other wire pairs in the cable. The crosstalk that appears on the left-hand side, $x_n(t)$ in
 681 wire pair i , is called near-end crosstalk (NEXT) because it is at the same end of the cable as the cross-
 682 talking signal source. The crosstalk that appears on the right-hand side, $x_f(t)$ in wire pair i , is called far-
 683 end crosstalk (FEXT) because the crosstalk appears on the end of the loop opposite to the reference
 684 signal source. In the loop plant, NEXT is generally far more damaging than FEXT because NEXT has a
 685 higher coupling coefficient and, unlike far-end crosstalk, near-end crosstalk directly disturbs the received
 686 signal transmitted from the far-end after it has experienced the propagation loss from traversing the
 687 distance from the far-end down the disturbed wire pair.

688 In a multi-pair cable, relative to the wire-pair the desired receive signal, all of the other wire pairs are
 689 sources of crosstalk. For DSL systems, the reference cable size for evaluating performance in the
 690 presence of crosstalk is a 50 pair cable [2]. So by reviewing the example shown in Figure 4, we see that
 691 relative to the received signal on wire pair i , the other 49 wire pairs are sources of crosstalk (both near-
 692 end and far-end).

693 **C.1.1. Near-end Crosstalk Model**

694 As described in references [2,3,5 and 6], for the reference 50 pair cable, the near-end crosstalk *coupling*
 695 of signals into other wire pairs within the cable is modeled as

696
$$|H_{NEXT}(f)|^2 = \chi_{49} \times \left(\frac{N}{49}\right)^{0.6} \times f^3$$

697
 698 where $\chi_{49} = 8.818 \times 10^{-14}$ is the coupling coefficient for 49 NEXT disturbers, N is the number of
 699 disturbers in the cable, and f is the frequency in Hz. Note that the maximum number of disturbers in a
 700 50 pair cable is 49. A signal source that outputs a signal with power spectral density $PSD_{Signal}(f)$ will
 701 inject a level of NEXT into a near-end receiver that is

702
$$PSD_{NEXT}(f) = PSD_{Signal}(f) \times |H_{NEXT}(f)|^2$$

703
 704 So as illustrated in Figure 4, if there are N signals in the cable with the same power spectral density
 705 $PSD_{Signal}(f)$, the PSD of the NEXT at the input to the near-end receiver on wire pair i is $PSD_{NEXT}(f)$.

706 Note from the above expressions that the crosstalk coupling is very low at the lower frequencies and the
 707 coupling increases at 15 dB per decade with increasing frequency. For example, at 80 kHz, the coupling

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708 loss is 57 dB for 49 disturbers. The loss (in dB) for 49 disturbers at other frequencies may be computed
 709 using the following formula:

710
$$L_{49} = 57 \text{ dB} - 15 \cdot \log\left(\frac{f}{80 \text{ kHz}}\right),$$

711 where L_{49} is the near-end crosstalk coupling loss in dB and f is the frequency in kHz.

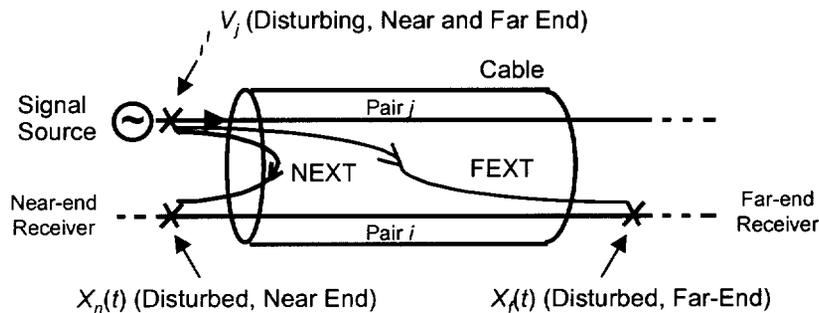
712 C.1.2. Far-end Crosstalk Model

713 Correspondingly, in the same 50 pair cable, the far-end crosstalk coupling of signals into other wire pairs
 714 is modeled as

715
$$|H_{FEXT}(f)|^2 = |H_{channel}(f)|^2 \times \left(\frac{N}{49}\right)^{0.6} \times k \times l \times f^2$$

716 where $H_{channel}(f)$ is the channel transfer function, $k = 8 \times 10^{-20}$ is the coupling coefficient for 49 FEXT
 717 disturbers, N is the number of disturbers, l is the coupling path length in feet, and f is the frequency
 718 in Hz.

719 Note that the coupling is small at low frequencies and large at higher frequencies. The coupling slope
 720 increases at 20 dB/decade with increasing frequency.



721

722 **Figure 4:** NEXT and FEXT in a multi-pair cable.

723

724 C.2. Applications that use Intermediate TU Devices

725 In some instances it may be desired to evaluate the effect of interference from systems that use
 726 intermediate (TU-I) devices between the CO and CI to another system. In these cases, the TU-I is
 727 integrated in to the same binder at some intermediate point between the CO and the CI such as may be
 728 the case in DLC deployments. In this case, crosstalk from the intermediate TU system will and affect the
 729 CO based system. The reverse is generally not of concern because the intermediate TU system benefits
 730 from higher signal levels as a result of the shorter path for the signals in the intermediate TU system.

731 The configuration in Figure 5 shows the sources of the crosstalk that are represented in the simulation
 732 model for the basis system downstream receiver.

733

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734 **C.2.1. Interference into the Basis System Downstream Receiver**

735 The model in Figure 6 should be used when performing a computer simulation of the effect of the new
736 technology intermediate TU-I system NEXT and FEXT interference into the basis system downstream
737 receiver.

738 Assumptions:

- 739 • The TU-I will integrate with the CO based binders at an intermediate point between the CO and the
740 CI, such as at the FDI (or SAI).
- 741 • The head-end transmitters (TU-Cs) for the two systems are not co-located.
- 742 • All customer premises transmitters (TU-Rs) for both systems are co-located.
- 743 • The binders are contiguous for the purposes of demonstrating spectral compatibility with the
744 exception of the TU-I integration

745 The first cable section is adjusted to cover the distance from the CO based TU-C to the intermediate TU-
746 I, (Z-D ft), and the second cable section is adjusted to cover the remaining length (D ft) of the test loop
747 under consideration. The new technology New TU-I FEXT noise is equivalent to the New TU-I output
748 signal passed through the FEXT coupling loss, using a coupling length equal to the second cable section
749 (labeled Z - Y - A + D ft). The resulting FEXT coupling equation for this second cable section is
750 expressed by

$$751 \quad |H_{FEXT}(f)|^2 = |H_{L1}(f)|^2 \times \left(\frac{N}{49}\right)^{0.6} \times k \times L2 \times f^2$$

752 where $H_{L1}(f)$ is the transfer function of the cable section from the New TU-I to the New TU-R, N is
753 the number of disturbers, $k = 8 \times 10^{-20}$ is the coupling coefficient for 49 FEXT disturbers,
754 $L2 = D = Z - Y - A$ is the coupling path distance in ft, and f is the frequency in Hz.

755 **C.2.2. Interference into the Basis System Upstream Receiver**

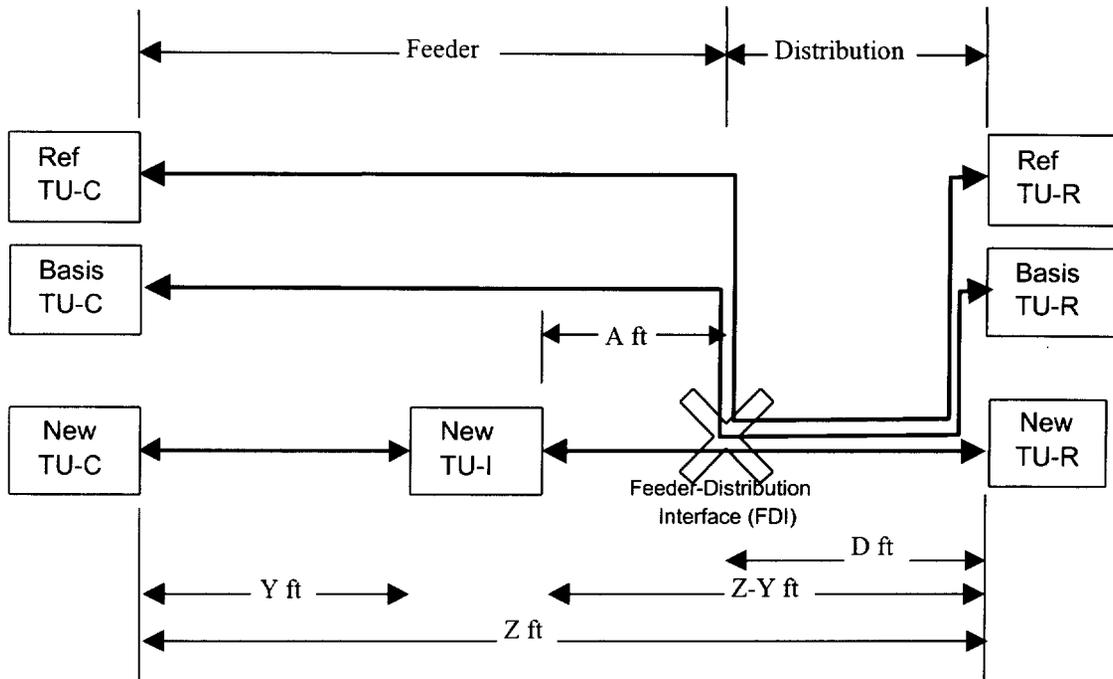
756 The model in Figure 7 should be used when performing a computer simulation of the effect of the
757 intermediate TU-C system new technology NEXT and FEXT interference into the basis system upstream
758 receiver.

759 Assumptions:

- 760 • The intermediate TU-I will integrate with the CO based binders at an intermediate point between the
761 CO and the CI.
- 762 • The head-end transmitters (TU-C) for the two systems are not co-located.
- 763 • The customer premises transmitters (TU-R) for both systems are co-located.
- 764 • The binders are contiguous for the purposes of demonstrating spectral compatibility with the
765 exception of the TU-I integration.

766 The first cable section is adjusted to cover the distance from the CO based TU-C to the TU-I, and the
767 second cable section is adjusted to cover the remaining length of the test loop under consideration. The
768 new technology NewTU-R FEXT noise is equivalent to a NewTU-R output signal passed through the
769 FEXT coupling loss, using a coupling length equal to the second cable section. The NewTU-R FEXT
770 noise is attenuated by the first cable length. The new technology New TU-C NEXT noise is determined
771 by the New TU-C output signal. The New TU-C NEXT noise is attenuated by the first cable length.

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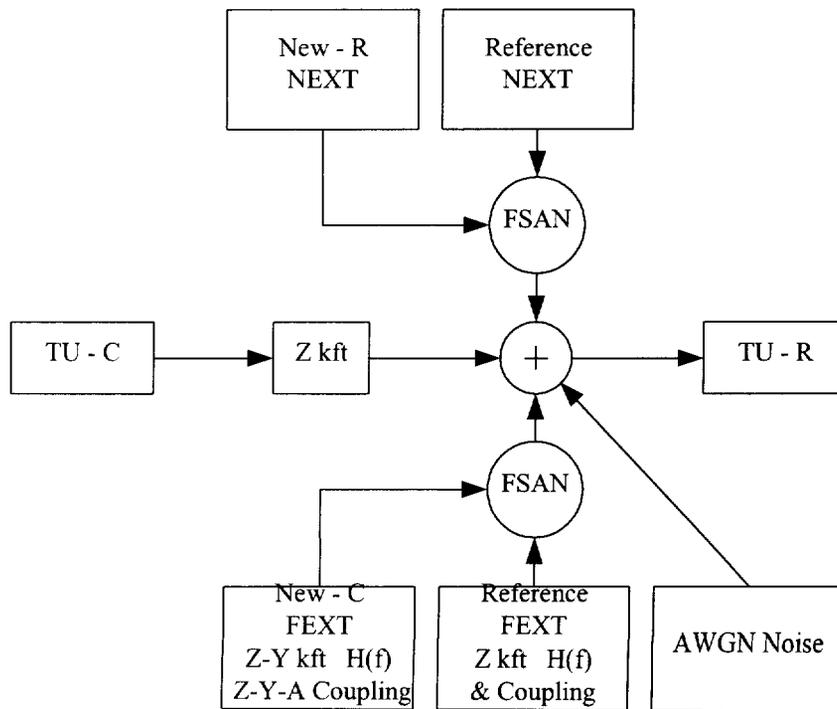


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Figure 5: NEXT & FEXT from Remote TU-C into TU-R.



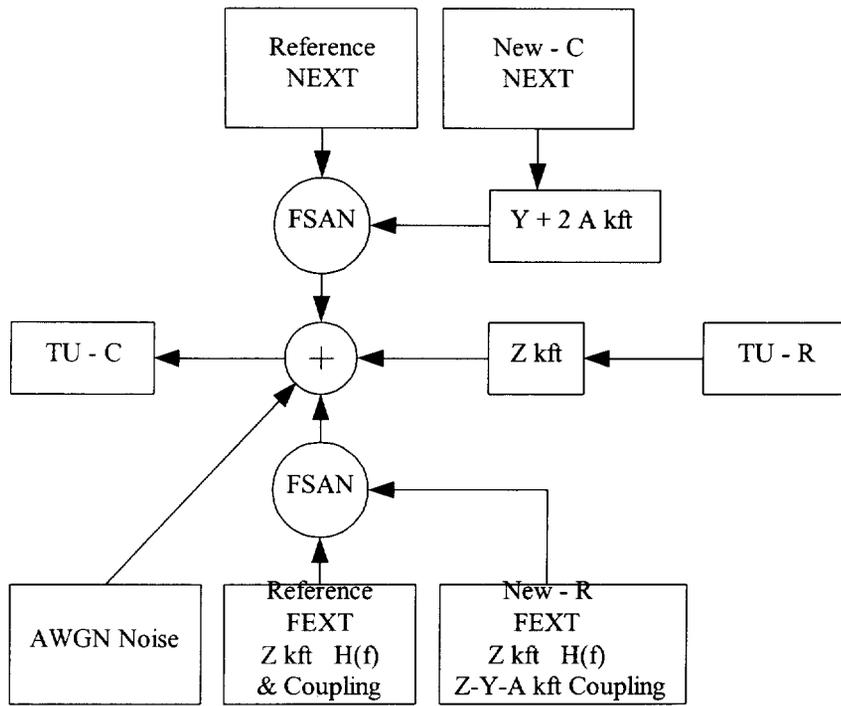
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Figure 6: Model for Reference and New Crosstalk into TU-R with Remote TU-C Device.

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Figure 7: Model for Reference and New Crosstalk into TU-C with Remote TU-C Device.

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